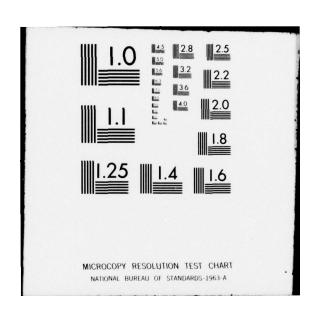
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SCHUYLKILL RIVER BASIN

LITTLE SCHUYLKILL DAM SCHUYLKILL COUNTY, PENNSYLVANIA NATIONAL I.D. NO. PA-00655

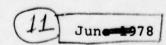
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PHASE I INSPECTION REPORT

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Submitted to:

DEPARTMENT OF THE ARMY Baltimore District, Corps of Engineers Baltimore, Maryland 21203



PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

Name of Dam: Little Schuylkill Dam County Located: Schuylkill County

State Located: Pennsylvania Stream: Little Schuylkill Creek

Coordinates: Latitude 40° 50.2' Longitude 76° 0.3'

Date of Inspection: 23 May 1978

Based on the visual inspection, available records and the short past operational performance of this dam, the dam is judged to be in good condition. The dam is owned by the County of Schuylkill and was designed by the Soil Conservation Service as a flood control dam. The purpose of this dam is to control Little Schuylkill Creek which passes through the downstream town of Tamaqua.

Evaluation of watershed data provided by the Soil Conservation Service and hydrologic data associated with the upstream Still Creek Reservoir indicates that the spillway is capable of passing a flood similar to the probable maximum flood. Therefore, the spillway is considered to be "Adequate" for this "High" hazard dam.

The visual observations did not indicate any existing embankment instability problems. There was some minor erosion noted on the up- and downstream slopes and one small seep was observed adjacent to the right abutment of the dam immediately above the impact basin. Both the erosion and seepage appear to be stable but the seepage should be monitored and the relationship between the reservoir head and seepage quantity established to determine if there is a variation with time. Visual inspection of the principal and emergency spillways did not reveal any evidence of deterioration or instability. There are no additional studies recommended.

Since there is no dam tender on-site, and since the dam does not store water except during floods, it is believed that continuous surveillance is not necessary. However, it is recommended that the dam be inspected during and after each severe storm to determine if a hazardous condition is developing. Since the structure does not impound water, there is the possibility that desiccation (shrinkage) cracks could develop in the structure. Therefore, it is recommended that the embankment slope be thoroughly inspected at least annually. Should shrinkage cracks develop, it is recommended that the crack area be scarified, regraded,

compacted and revegetated. The inspection program should also check for vandalism and overall deterioration of the dam and appurtenant structures. The Owner should develop a maintenance inspection checklist to help insure that all critical items are inspected. A formal warning system should be developed for use in the event an emergency is noticed during the time the dam stores and passes large flows.

John H. Frederick, Jr., P.E Maryland Registration 3701

William S. Gardner, P.E.

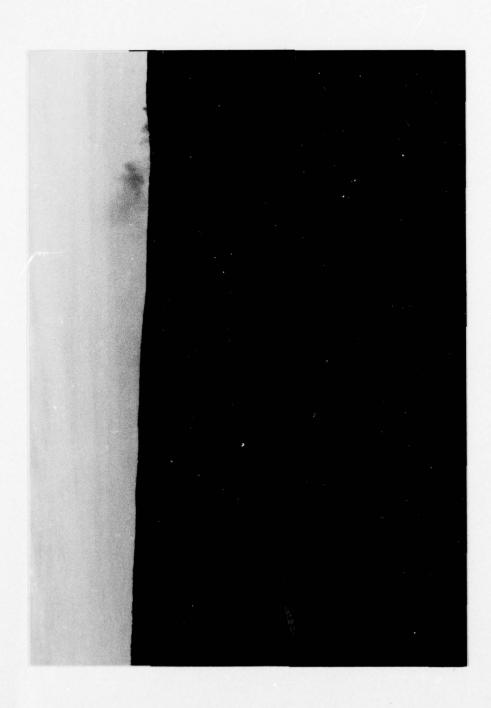
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APPROVED BY:

OHN H. KENWORTHY

OTC, Corps of Engineers

Acting District Engineer



OVERVIEW COUNTY, PENNSYLVANIA

PHASE 1 INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM
LITTLE SCHUYLKILL DAM
NATIONAL ID #PA 00655
DER ID #54-174

SECTION 1 PROJECT INFORMATION

ARSTRACT

1.1 General.

- a. Authority. The Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of inspection of dams throughout the United States.
- b. Purpose. The purpose of the inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 Description of Project.

Dam and Appurtenances. Little Schuylkill Dam is a zoned rolled earth dam with a downstream drainage trench and drainage blanket. The dam is approximately 700 feet long and 87 feet high, measured from the streambed to the crest. The dam was designed to use available borrow materials derived within the reservoir area. The interior zone (Zone 1) is reportedly composed of sandy clays and gravelly clays. The exterior zone (Zones 2 and 3) materials are reportedly composed of gravelly clays and silty gravels, respectively.

Underseepage is controlled by a cutoff trench located approximately 80 feet upstream of the centerline of the dam. This trench is 40 feet wide at the base with 2H:1V slopes from the base of the trench to the stripping line elevation. The dam also contains a triple-line staggered grout curtain. Holes are spaced longitudinally 10 feet on-center and five feet up and downstream of the centerline. The upstream section has a riprap facing from the toe of the dam to elevation 1071, with a gravel filter layer between the Zone 2 embankment materials and the riprap protection.

Water is released from the dam through the principal spillway comprised of a two-stage reinforced concrete riser located at the upstream toe and a 48-inch reinforced concrete pipe. The outlet pipe discharges into an impact basin at the downstream toe. The stream flow normally passes through the lower intake orfice. If impoundment levels reach elevation 1048, additional flow is discharged through the upper weir. Thereafter, water is stored behind the structure until it reaches the emergency spillway elevation of 1103.0. The emergency spillway is located in the right abutment.

- b. Location. The dam is located on the Little Schuylkill Creek approximately 3.2 miles north-northwest of the town of Tamaqua. The dam, reservoir, and drainage basin are located in Schuylkill, Carbon and Berks Counties, Pennsylvania. The dam was built concurrently with Neifert Creek Dam, located 800 feet west of Little Schuylkill Dam. The dam site and reservoir are shown on USGS Quadrangle Delano, Pennsylvania, at coordinates N 40° 50.2', W 76° 0.3'. A Regional Location Plan of Little Schuylkill Dam is enclosed as Plate 1, Appendix E.
- c. <u>Size Classification</u>. The dam is classified as "Intermediate" by virtue of its 87 foot height.
- d. Hazard Classification. "High" hazard because of the potential for extensive property damage and possible loss of life to the downstream town of Tamaqua, should the dam fail.
 - e. Ownership. Schuylkill County Commissioners.
 - f. Purpose of Dam. Flood control.
- g. Design and Construction History. Little Schuylkill Dam was built as a flood retarding structure under the provisions of the Watershed Protection and Flood Prevention Act. It was designed by the Soil Conservation Service (SCS) and constructed by S.J. Groves Company. Construction began on October 10, 1967. Final design drawings and specifications were prepared by the SCS.

The Resident Engineer for the SCS during construction was Mr. John Mickley. The SCS inspectors were Messrs. Byron Roth and Eugene LaBar.

By September 5, 1968, the Contractor, S.J. Groves Company had finished topping out the 87 foot high embank-ment. At that date it was reported that the only work remaining was some rock excavation in the emergency spillway. Based on available records discussed in subsequent sections, it is concluded that the dam was built in accordance with the design drawings.

h. Normal Operating Procedures. As a "dry" flood control structure not designed for permanent water impoundment, normal flow passes directly into the lower intake of the concrete riser (see Plate 2) and is discharged downstream. During a storm, water is released at a controlled rate through the intake riser at two intake elevations. All other water is temporarily stored behind the embankment. During rare, exceptionally high flows, the system was designed to pass excess water over the emergency spillway located in the right abutment of the dam.

1.3 Pertinent Data.

A summary of pertinent data is summarized as follows:

a.	Drainage Area (sq. miles)	15.6
b.	Maximum Known Flood at Dam (June, 1972) Principal Spillway (Water	2 feet below emergency spillway. Crest (Elev. 1101)
	at Emergency Spillway Crest) Combined Discharge at Maximum	320
	Pool (Elev. 1116.6)	37,500
c.		
	Top of Dam (after settlement)	1116.6
	Normal Pool	Dry
	Maximum Pool Possible	1116.6
	Maximum Pool of Record (June,	
	1972)	1101
	Principal Riser	
	Lower (Pond Drain)	1028.0
	Upper	1048
	Emergency Spillway Crest	1103
	Exit Invert of Principal	
	Spillway	1024.9

d.	Reservoir (miles) Length at Elev. 1103 Length at Normal Pool	1.7 None
e.	Storage (acre-feet) Normal Pool (Elev. 1028) Maximum Pool	None
	Crest of Emergency Spillway At PMF Elevation	3698 6000
f,	Reservoir Surface (acres) Normal Pool	None
g.	Dam Data Type	Rolled earth with down-
		stream drain
	Length	700 feet
	Height above streambed	87 feet
	Crest width Volume	25 feet
	Side Slopes	452,580 cubic yards
	Upstream Crest to El. 1072	2.89H:1V
	From El. 1072 to toe	3.85H:1V
	Downstream	2.41H:1V
	Benches	2.41h:1V
	Upstream slope has two benches	
	Width at Elev. 1072	25 feet
	Width at Elev. 1049	12 feet
	Downstream slope has one bench	
	Width at Elev. 1060	12 feet
	Cutoff	Two 40 foot wide cutoff trenches from 10+50 to 17+60 located approxi- mately 80 U/S of center- line
	Grout Curtain	Triple line, staggered 10' on-center spacing. Spaced 5 feet U/S and D/S of centerline

CONTRACTOR NAME OF THE PARTY OF

h. Diversion and Regulating Facilities
Diversion

Closure Access

Regulating Facility

i. Spillway
Principal
Type
Size - Upper
- Lower
Discharge Conduit
Size (Diameter)
Length
Emergency
Type

Width at Control Section Downstream Channel Streambed was used for diversion while the principal spillway was constructed.

None
Only to intake and outlet structure of principal intake riser.

a) Intake riser pond drain inlet weir continuously drains reservoir: 3.5' x 4.0' inlet
b) Excess flow passes into upper inlet with a 4.0' x 12.0' inlet

Concrete intake riser 4.0' x 12.0' 4.0' x 3.5'

48 inch (RCP) 610 feet

The same of the sa

Channel excavated into rock 200 feet Both Spillways discharge into the natural stream channel which has a gravel and rock bottom.

SECTION 2 ENGINEERING DATA

2.1 Design.

a. Data Available. A summary of engineering data on Little Schuylkill Dam is attached as Appendix A. Engineering data available for Little Schuylkill Dam was contained primarily in a 23-page set of half-size drawings provided by the United States Department of Agriculture, Soil Conservation Service. In addition, a 20-page set of full-size drawings, and flood routings, prepared by the U.S. Department of Agriculture, Soil Conservation Service, were on file at the Department of Environmental Resources main office in Harrisburg, Pennsylvania. Department of Environmental Resources (DER) files also contain a set of construction specifications.

The SCS archives located in Mechanicsburg, Pennsylvania, contain complete files on the design and construction of the dam including the following: Soil Mechanics and Geology reports, design folder, drawings, and construction documentation including daily records, field testing results for both concrete and embankment construction. All other pertinent documents available and reviewed are listed in Appendix A.

b. Design Features. The principal design features of Little Schuylkill Dam are illustrated on the plans and profiles enclosed in Appendix E as Plates 2 through 7. These plates were reproduced from SCS drawings. The drawings show the embankment to have a maximum height of 87 feet. The dam contains a central impervious core of sandy clays and gravelly clays with exterior zones of gravelly clayey sandy silts. The downstream section contains an interior drainage blanket and drainage trench. The upstream section contains a riprap layer over a filter material from the toe of the dam to elevation 1071.0.

Underseepage is controlled by a grout curtain and a 40-foot wide cutoff trench located approximately 80 feet upstream of the centerline of the dam. The tripleline stagger spaced grout curtain is constructed along the centerline of the emergency spillway and along a portion of the embankment zone.

The as-constructed upstream slope is 2.98H:1V from the crest to elevation 1072. From elevation 1072 to elevation 1071, the upstream slope has a 25-foot wide berm. Below elevation 1071, a 3.85H:1V slope continues to elevation 1049.0. Between elevations 1049 and 1048, a 12-foot wide berm was constructed. Thereafter, a 3.85H:1V slope continues to the toe of the dam.

The downstream slope is 2.41H:1V to elevation 1061.0 with a 12-foot wide berm sloping to elevation 1060.0. Below elevation 1060.0, the slope is 2.41H:1V to the toe of the dam. Design features of the reinforced concrete intake riser and emergency spillway are shown on Plates 5 and 6 and discussed in Section 1.2.

2.2 Construction.

Details of construction are presented in Section 1.2, paragraph g.

2.3 Operation Data.

As a "dry" flood control structure, the design of Little Schuylkill Dam allows all water to be released. During high flows, this release is controlled by the intake system built into the concrete riser and the emergency spillway on the right abutment. There are no staff gages or recording equipment nor are records of water surface elevations maintained. The dam is accessible during high flow periods and it is reported that reservoir water surface elevations are monitored by the local Civil Defense Unit.

2.4 Evaluation.

a. Availability. All engineering data evaluated and reproduced for this report was provided by either the Pennsylvania Department of Environmental Resources or the Soil Conservation Service. Supplemental data including the complete design analysis and as-built documentation, together with construction records are available through the SCS State Office in Harrisburg, Pennsylvania.

- b. Adequacy. Although the design data which exists and computed by the Soil Conservation Service is comprehensive and well-documented.
- c. Validity. Design drawings showed the proposed borrow source to be located within the reservoir area. Discussions with the Owner's representative confirmed the use of these borrow materials. Based on the visual inspection and the ten photographs available, together with the design drawings, it is judged that the dam and appurtenances were most likely constructed as designed.

SECTION 3 VISUAL INSPECTION

3.1 Findings.

- a. General. The observations and comments of the field inspection team are contained in the checklist enclosed herein as Appendix B, and are summarized and evaluated as follows. In general, the appearance of the facility, based on the visual inspection and comparison with the design drawings, shows that the dam and its appurtenances were constructed in accordance with the drawings. The dam and appurtenances appear to be in good condition.
- b. <u>Dam</u>. During the visual survey, there were no indications or evidence observed of distortions in alignment or grade that would be indicative of movement of the embankment or the foundations. Some minor erosion was observed on the up- and downstream slopes, however, the slopes are vegetated with crown vetch and presently appear to be stable.

A careful inspection of the upstream slope disclosed no evidence of seepage emergence. Some seepage was observed within the reservoir area and is typical of natural seepage patterns throughout the region. No downstream seepage was observed along the left abutment of the dam. Only one very slight seep was observed along the right abutment of the dam, approximately 50 feet upstream from the discharge impact basin. In general, the dam appears to be in good condition.

c. Appurtenant Structures. At the time of this inspection, the water level was at the base of the control riser. Some debris has accumulated around the riser allowing the water to back-up approximately one foot. It is understood from the Owner's representative that a local contractor cleans this riser at least once per year. Debris was noted on the top of the riser, indicating that flood waters had inundated the riser to an elevation of at least 1050 prior to the last clean-up. All appurtenant structures were inspected and observed to be in good condition.

- d. Reservoir. Reconnaissance of the reservoir disclosed no evidence of significant siltation, slope instability, or other features that would significantly effect the flood storage capacity of the reservoir. One minor surficial slope slide was observed on the reservoir slope near the left abutment of the dam. At the base of this slide, a small seep was noted. Typical for this area, it is believed that sidehill seepage at this location caused the slide.
- e. <u>Downstream Channel</u>. As shown on Photo No. 6, the downstream channel is predominantly rock and gravel lined. Both sides of the channel below the impact basin are heavily wooded and densely covered with vegetation.

3.2 Evaluation.

No evidence of apparent, past or present movement to indicate instability of the dam or embankment during periods of retention was detected. The inspection revealed that the overall condition of the dam and appurtenances is good. The only feature of note detected was a small seep emerging near the base of the dam above the impact basin. This seep should be watched during subsequent investigations. If seepage increases or becomes turbid, remedial action is recommended.

SECTION 4 OPERATION PROCEDURES

4.1 Procedures.

Little Schuylkill Dam is a "dry" flood retention structure which controls the rate of storm water runoff by means of a two-stage vertical concrete riser and an emergency spillway. Under normal stream flow conditions, all water is discharged into the lower intake of the concrete riser and passed through a 48-inch reinforced pipe located below the dam. The pipe discharges into an impact basin and the flow subsequently enters the natural streambed.

During high flow conditions, the water passes through the lower intake at a controlled rate while excess water is stored behind the embankment. When the water level rises and reaches the upper weir at elevation 1048, the discharge increases significantly. Water is stored in the reservoir until the impoundment level reaches the crest of the emergency spillway at elevation 1103. Flow over the emergency spillway is discharged into the downstream channel immediately below the impact basin. All systems are ungated and do not require an attendant. It is to be noted that the riser crest (elevation 1048) was set at the top of the estimated 50-year sedimentation accumulation.

4.2 Maintenance of the Dam.

The dam is owned by the Schuylkill County Commissioners who contract maintenance to a local contractor. The contractor cleans the intake riser yearly and performs other maintenance of the dam and reservoir as deemed necessary by the Schuylkill County Commissioners. There are no official maintenance procedures available. It is reported that the dam is inspected prior to each maintenance and the contractor is given instructions as to the work to be completed.

4.3 Maintenance of Operating Facilities.

Since the operating facilities are all ungated, maintenance consists of inspecting the structures for debris collection around the intakes.

4.4 Warning Systems in Effect.

There are no formal warning systems or procedures established to be followed during periods of exceedingly heavy rainfall. During high flows, access to the dam for inspection can be gained from the left abutment. It is reported that the local Civil Defense Unit monitors the structure during periods of heavy rainfall.

4.5 Evaluation.

Since the dam does not store water permanently, the embankment could not be inspected to evaluate how it would respond under reservoir loading conditions. There is no evidence to indicate that hazardous conditions develop during this short retention period. Since there is no attendent on-site, it is recommended that a formal warning procedure be implemented during periods of extreme rainfall. It is also recommended that a maintenance procedure and checklist be formulated to assure that all items are periodically checked, including the downstream seep noted in Section 3.

SECTION 5 HYDROLOGY/HYDRAULICS

5.1 Evaluation of Features.

a. Design Data. Original available design data was limited to statements located in the State Files, particularly in the Application Report, dated June 2, 1966, and flood routings performed by the Soil Conservation Service. Subsequently, the SCS files were reviewed. The watershed contains an upstream dam and reservoir, Still Creek. The latest USGS maps indicate a drainage area of 6.9 square miles for Still Creek versus the 8.7 square miles used in SCS flood routing. Still Creek watershed is long and narrow, approximately 3.8 miles long and 1.4 to 2.4 miles wide, the long direction being east-west. Still Creek Dam is located approximately 2.3 miles upstream and east of Little Schuylkill Dam.

The north-south portion of Little Schuylkill Dam watershed is approximately 3.7 miles long. The shape of the watershed is funnel-shaped, with the east-west portion about 9 miles (including Still Creek drainage basin). The width of the watershed 4,000 feet above the dam is approximately 2.1 miles. The elevations range from 1950 on Spring Mountain to 1130 feet at the upstream toe of the dam. The watershed is mountainous, about 90 percent wooded, sparsely populated and with some new housing. It is not expected that the area will experience rapid growth although the possibility exists that strip mining may alter the watershed characteristics.

Original spillway capacity calculations rate the spillway to be capable of discharging a total of 13,700 cfs at design high water (elevation 1111.3 feet). Combined spillway capacity with the reservoir level at the top of the dam is rated as 37,550 cfs. In accordance with the criteria established by the Federal (OCE) Guidelines, the recommended spillway design flood for this "Intermediate" size dam and "High" hazard potential classification is the probable maximum flood (PMF).

b. Experience Data. Reservoir water surface elevations during floods are not measured and no records are maintained. It was reported by a local resident that the

water level in the reservoir during Hurricane Agnes (June 1972) was two feet below the emergency spillway crest, which would result in an estimated discharge of 350 cfs through the principal spillway system. The June 1972 storm produced 5.28 inches of rain recorded at the upstream Still Creek Dam.

- c. <u>Visual Observations</u>. On the date of the inspection, no conditions were observed that would indicate that the outlet capacity would be significantly reduced during a flood occurrence. Observations regarding the downstream channel, spillway condition and reservoir are located in Appendix B.
- Overtopping Potential. Analysis of the overtopping potential of Little Schuylkill Dam required evaluation of the upstream Still Creek Dam. A design storm and a freeboard storm, which approximates the PMF, were routed through Still Creek by the Soil Conservation Service (SCS). The Still Creek storms were developed using a drainage area of 8.7 square miles, which is not supported by current USGS maps (6.9 square miles). Therefore, the calculated peak inflow of the routed storms is greater than it should be as is the routed peak outflow from Still Creek. The SCS Still Creek routings indicate the design storm passes through Still Creek reservoir with two feet of free-The SCS freeboard (PMF) routing indicates the dam will be overtopped. However, no statement as to the overtopping of Still Creek Dam is made in any reports, correspondence, etc., available for review. The Still Creek spillway was judged "Adequate" for the following reasons:
 - The drainage area used in PMF storm development is too large;
 - SCS procedures are known to be conservative for small watersheds; and
 - Still Creek Dam Spillway is capable of passing a PMF peak inflow as estimated from a similar watershed.

The inflow hydrographs developed for Little Schuylkill Dam (shown in Appendix C) consist of the routed outflow from Still Creek Dam (peak PMF discharge of 22,200 cfs, conservatively assuming time lag), added to the intervening area inflow hydrograph (peak PMF inflow of 16,700 cfs) for a total peak PMF inflow of 38,200 cfs. This storm was routed and the top of the dam was set equal to the maximum reservoir water level. The intervening area hydrograph was developed based on an area of 6.88 square miles, less than the 7.79 square miles determined from USGS maps and, therefore, is slightly smaller than it should be. As the total drainage area contributing to Little Schuylkill Dam (as disclosed by current USGS maps) is less than the total area used in the hydrologic analysis. The expected peak PMF inflow would be somewhat less than 38,200 cfs, and, therefore, the dam will not be overtopped.

- e. Spillway Adequacy. Based on the available information, the spillway is judged "Adequate". The two-stage discharge system (principal and emergency spillways) and the upstream reservoir are not suitable for the flood routing technique suggested by the January 25, 1978, Preliminary Engineer Technical Letter No. 1110-2 and, therefore, the judgement of spillway adequacy is qualitative rather than quantitative. The tailwater is estimated to be approximately 50 feet below the crest of the dam during passing of the PMF.
- Downstream Conditions. Little Schaylkill Dam is a flood control structure built in conjunction with the Neifert Creek Dam, located approximately 800 feet west of Little Schuylkill Dam. The drainage area controlled by Neifert Creek Dam is approximately 3.1 square miles. Little Schuylkill joins Neifert Creek approximately 1,000 feet downstream of Little Schuylkill Dam. The channel passes through a 400-foot wide, wooded flood plain. Approximately 3,000 feet downstream of the dam is the Central New Jersey Railroad tressel. (See Photographs 5 and The tressel is not likely to significantly obstruct large flow although the possibility exists that the tressel piers would be damaged by debris if the dam failed. The potential for downstream damage was estimated by the SCS in the watershed work plan dated April, 1958. A section of this work plan is quoted as follows:

"Severe flooding damage occurs periodically at Tamaqua (population 12,000), at Reynolds, location of the Atlas Powder Company, and on several other reaches along the river. Flooding damages start between a 5- and 10-year frequency of occurrence. The high stream gradient produces velocities capable of causing great damage even at bank-full stages to the Reading Railroad's main branch along the Little Schuylkill River".

Consistent with the "High" hazard potential classification of this structure, significantly more damage, including loss of life, would occur if the structure failed during the PMF than if it did not fail during the PMF.

SECTION 6 STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability.

- a. <u>Visual Observations</u>. The visual observations did not indicate any existing embankment stability problems. There are some minor erosion gullies noted on the up- and downstream slopes, however, these have been overgrown with vegetation and are currently stable. The only seepage observed was a small seepage zone located along the right abutment upstream of the impact basin. Evidence of vegetation around the seep and of the seep itself indicates that it is most likely sidehill seepage and not associated with seepage from the reservoir. It is not believed that remedial action is necessary.
- b. Design and Construction Data. Available design documentation included a series of design drawings prepared by the Soil Conservation Service for this project and a complete set of design computations are on file at the Soil Conservation Service office in Mechanicsburg, Pennsylvania.

Photographs of the construction tend to confirm that proper placement and zoning were performed. It is also noted that the Soil Conservation Service had representatives on-site throughout the construction period. Since the photographs confirmed the existence of the interior design features and the inspection confirmed the exterior design features, coupled with the fact that Soil Conservation Services' representatives were on-site, it is believed that the construction was performed in accordance with the plans and specifications.

- c. Operating Procedures. Since the dam has been designed to only temporarily retain water and control the rate of flow downstream by an unmanned regulatory system, there are no records available.
- d. <u>Post-Construction Changes</u>. There are no reports nor is there any evidence that modifications were made to this dam. The design and as-built drawings were available and compared. There were no major modifications observed.

e. Seismic Stability. This dam is located in Seismic Zone 1. Normally, it can be considered that if a dam in this zone is stable under static loading conditions, it can be assumed safe for any expected earthquake conditions. Since the static stability analysis could not be reviewed, the seismic stability of the dam could also not be evaluated.

SECTION 7 ASSESSMENT/REMEDIAL MEASURES

7.1 Dam Assessment.

a. Assessment. The visual inspection and review of the design documentation indicates that the dam embankment, foundation and appurtenant structures of Little Schuylkill Dam are in good condition. The involvement of the SCS in design and construction also suggests that the dam is adequately designed and constructed.

The hydrologic and hydraulic routings included in the available design documents indicated that this structure will pass the PMF. Therefore, the discharge systems of the structure are considered "Adequate". It is noted that although the structure has been designed to pass the PMF, significant property damage potential is likely to the downstream town of Tamaqua if a catastrophic failure of the embankment occurred while retaining a portion of the PMF.

- b. Adequacy of Information. It is judged that the information available for the purpose of the prescribed inspection program was adequate.
- c. <u>Urgency</u>. It is considered that recommendations suggested be implemented during the routine maintenance work. Recommendations for written procedures should be performed as soon as practicable.

7.2 Remedial Measures.

- a. Considering the results of this inspection, specific remedial measures recommended are as follows:
 - The log currently wedged at the base of the entrance tower should be removed.
 - 2. It is recommended that the Owner monitor the downstream seep, especially after periods of retention behind the embankment.

- 3. A relationship should be established between the reservoir head and the quanities of seepage existing on the right side of the dam. If the relationship between the seepage quanities and the reservoir pool is found to increase with time or the seepage becomes excessive or turbid, appropriate measures should be taken.
- b. Operation and Maintenance Procedures. Because of the location of the dam upstream from the populated area of Tamaqua, a formal procedure of observation and warning during periods of high precipitation should be developed and implemented. The Owner should develop a maintenance checklist to insure that all critical items are inspected on a periodic basis. It is recommended that the trash racks be kept thoroughly cleaned to prevent clogging of the system.

APPENDIX

A

Sheet 1 of 4

DESIGN, CONSTRUCTION, OPERATION PHASE I ENGINEERING DATA CHECK LIST

NAME OF DAM Little Schuylkill PA 00655

QI

REMARKS

None available. SCS 1/2 size design drawings were available, 23 sheets. SCS full size drawings were also available, 15 sheets, # PA-422A-P. AS-BUILT DRAWINGS

This data was included in the SCS design drawings. REGIONAL VICINITY MAP None in DER files, but several miscellaneous letters inferred the state of progress. Two sets of field books, "Job Diary" and "Constructions Records" are on file in SCS archives, Mechanicsburg, Pernsylvania. CONSTRUCTION HISTORY

This data was included in the SCS design drawings. TYPICAL SECTIONS OF DAM

OUTLETS - PLAW

This data was provided with the SCS design drawings.

DETAILS

CONSTRAINTS

DISCHARGE RATINGS

RAINFALL/RESERVOIR RECORDS

None available other than data upstream at Still Creek Reservoir.

Design reports. A copy of the prepared specifications is contained in the DER files. located in SCS archives. REMARKS DESIGN REPORTS ITEM

GEOLOGY REPORTS None in DER files, located in SCS archives.

DESIGN COMPUTATIONS
HYDROLOGY & HYDRAULICS
UAM STABILLITY
SEEPAGE STUDIES

Preliminary storm routing data provided on 4 SCS sheets dated 1963 and 1964. (1)

(2) Design computations were referenced in a letter dated June 6, 1966 to Mr. Lunetta from Mr. Right (SCS) but data was not in DER files.

(3) Complete design computations located in SCS archives.

MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD

Logs of drill holes presented on Drawing PA-422-P, sheets 14 through 18 sheet 4 of 20 dated May, 1966, entitled " Profiles of Dam and Emergency Spillway". Dam profiles and borings are presented on SCS design drawing PA-422-P, (1) (2)

Soil compaction data presented on Drawing PA-422-P, sheet 20 of 20 dated May, 1966. of 18. (3)

POST-CONSTRUCTION SURVEYS OF DAM None.

BORROW SOURCES

Data provided on SCS design drawing PA-422-P, sheet 2 of 20 dated May, 1966, entitled "Plan of Storage Area".

ITEM

REMARKS

MONITORING SYSTEMS None.

MODIFICATIONS None.

HIGH POOL RECORDS None.

None. Only a few from inspection reports. POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS

PRIOR ACCIDENTS OR FAILURE OF DAM None. DESCRIPTION REPORTS

None. The structure is used solely as a flood control structure and does not retain water. MAINTENANCE OPERATION RECORDS REMARKS Data provided on SCS drawings. SECTIONS DETAILS SPILLWAY PLAN ITEM

None other than open spillway and intake structure. OPERATING EQUIPMENT PLANS & DETAILS The DER files contained several (8 to 12) black and white photos of construction and post construction Pennsylvania State (DER) inspection records. **PHOTOGRAPHS**

APPENDIX

B

THE PARTY OF THE P

CHECK LIST VISUAL INSPECTION PHASE I

									National		
Name Dar	n Little Su	shuy lkil	11 River	. Dam	County	Name Dam Little Schuylkill River Dam County Schuylkill	State Pe	State Pennsylvania	# QI	ID # PA 00655	- 1
Type of	Type of Dam Rolled Earth	ed Earth		1		Hazard Category I (High)	I (High	1)			
Date(s)	Date(s) Inspectión <u>23 May 197</u> 8	23 May	1928	Weath	Weather Mild		Temperature 65°F	65°F			
Pool Ele	Pool Elevation at Time of Inspection 1028 M.S.L.	Time of	Inspect	rion	8201		er at Time	Tailwater at Time of Inspection 1025.4 M.S.L.	1025.4	M.S.L.	

Inspection Personnel:

Vincent McKeever (Hydrologist) Raymond Lambert (Geologist) John Frederick (Geotechnical) John Boschuk (Geotech/Civil) Marry Beck (Hydrologist)

John Boschuk, Ir. Recorder

Remarks:

Mr. Hugo Subrime - Owner's representative was on-site and provided assistance, as necessary.

CONCRETE/MASONRY DAMS

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
ANY NOTICEABLE SEEPAGE	N/A	
STRUCTURE TO ABUTMENT/EMBANKMENT JUNCTIONS	N/A	
DRAINS	N/A	
WATER PASSAGES	N/A	
FORUDATION		

N/A

CONCRETE/MASONRY DAMS

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SURFACE CRACKS CONCRETE SURFACES	N/A	
STRUCTURAL CRACKING	N/A	
VERTICAL AND HORIZONTAL ALIGNMENT	N/A	
MONOLITH JOINTS	N/A	
CONSTRUCTION JOINTS		

N/A

EMBANKMENT

REMARKS OR RECOMMENDATIONS OBSERVATIONS None observed. VISUAL EXAMINATION OF SURFACE CRACKS

UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE

None observed.

SLOUGHING OR EROSION OF EMBANIMENT AND ABUTHENT SLOPES

Some minor erosion was observed on the downstream slopes and abutments as a result of motor bike traffic. On the upstream slope, grass covered gullies up to 12 inches deep and 15 inches wide were observed. These D/S gullies appear to be old and relatively stable.

VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST

No unusual movement was observed.

RIPRAP FAILURES

None observed.

EMBANKMENT

REMARKS OR RECOMMENDATIONS A small hillside slope failure was noted in the left abutment on the upstream side of the embankment. The slope failure was in natural material, not on the embankment. A seep emerges from the toe of the slope slough and is probably responsible for the failure. The slough measures about 15 to 20 feet in diameter with a 10 to 12 OBSERVATIONS foot depth. VISUAL EXAMINATION OF ABUTMENT OBSERVATION

JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM

No significant erosion or other deterioration features were observed.

the right abutment on the downstream side. Moss is growing in the area and is shown on Photo 8, Appendix D. Other noted seepage was in the reservoir area eminating from Only one significant seepage zone was noted at the junction of the dam and several zones near the stream channel. ANY NOTICEABLE SEEPAGE

STAFF GAGE AND RECORDER

None

VEGETATION

These should Some woody vegetation, including trees, are starting to grow on the slopes. be removed as soon as practicable.

DRAINS

None observed.

OUTLET WORKS

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT	The only portion of the outlet structure that was visible was the pipe outfall in the baffle wall structure. It appeared to be in good condition. The rest of the pipe is buried in the dam.	was visible was the pipe outfall be in good condition. The rest
INTAKE STRUCTURE	Two stage reinforced concrete riser, each stage protected by a trash rack. Lower stage had 3 ft. diameter, 8 to 10 ft. long log and other debris wedged against trash rack and upper trash rack had debris on top. There was no spalling or significant deterioration observed.	ge protected by a trash rack. mg log and other debris wedged ebris on top. There was no 1.
OUTLET STRUCTURE	A four ft. reinforced concrete pipe, 609 ft. long, discharging into an impact basin. At time of the inspection, the pipe was flowing greater than one-half full and the system appeared to be performing satisfactorily. The baffle wall and outfall structure appeared to be in good condition.	long, discharging into an impact us flowing greater than one-half satisfactorily. The baffle wall condition.
OUTLET CHANNEL	Outlet channel is riprapped for approximately 50 ft. downstream of the impact basin. No erosion in either riprapped channel or natural channel further downstream was observed.	50 ft. downstream of the impact 1 or natural channel further

None.

EMERGENCY GATE

UNGATED SPILLWAY

EMERGENCY SPILLWAY

VISUAL EXAMINATION OF

CONCRETE WEIR

OBSERVATIONS

REMARKS OR RECOMMENDATIONS

may result in localised rock falls in the spillway area. Also the sandstone is blocky and—can fall into the spillway area from near-vertical rock cuts. None. The spillway is approximately 200 feet wide and is out into the rock through the right abutment. The bedrock which makes up the emergency spillway base and portion of the right (west) abutment is the shaley member of the Pocono Formation. This rock slakes and

About 100 feet long with approximately two percent reverse grade. Rock talus forming at base of right wall at several locations, not expected to reduce flow significantly during large flows. Few trees up to 4 to 5 years old at entrance to channel. Should be removed. APPROACH CHANNEL

Ine channel section is cut through the right abutment and is approximately 200 feet long with a 2½ percent grade. Thereafter the channel drops abruptly at an approximately 60 percent slope and drains into the natural creek channel. DISCHARGE CHA:INEL

Y tressel approximately 1700 feet downstream. None. However, there is a railroad photo can be found in Appendix D. BRIDGE AND PIERS

Sheet 8 of 11

GATED SPILLWAY

VISUAL EXAMINATION OF	0BSERVATIONS	REMARKS OR RECOMMENDATIONS
CONCRETE SILL		
None		

APPROACH CHANNEL

None

DISCHARGE CHANNEL

None

BRIDGE AND PIERS

None

GATES AND OPERATION EQUIPMENT

None

INSTRUMENTATION

Sheet 9 of 11

REMARKS OR RECOMMENDATIONS OBSERVATIONS None None None MONUMENTATION/SURVEYS VISUAL EXAMINATION OBSERVATION WELLS WEIRS

OTHER

None

PIEZOMETERS

None. A rain gage can be located upstream at Still Creek Reservoir (National I.D. No. PA 00700, State DER ID 54-111).

REMARKS OR RECOMMENDATIONS

VISUAL EXAMINATION OF

Little Schuylkill is a dry dam, the reservoir side slopes are moderate to steep, stable, well vegetated. OBSERVATIONS

SLOPES

SEDIMENTATION

A minimal amount of sedimentation was observed in the reservoir which would not reduce the design flood water storage capacity. There is some debris noted along the reservoir which marks the flood high water line.

DOWNSTREAM CHANNEL

REMARKS OR RECOMMENDATIONS OBSERVATIONS VISUAL EXAMINATION OF

CONDITION (OBSTRUCTIONS, DEBRIS, ETC.)

The only major obstruction noted downstream is the steel railroad tressel about 1700 feet downstream of the outfall structure. The flood plain as shown on Photo 6 is heavily wooded.

SLOPES

Side slopes appear to be stable and wooded to the channel bank. The valley gradient is approximately one percent or less.

APPROXIMATE NO. OF HOMES AND POPULATION

Approximately 4.5 miles downstream there are a large number of houses and businesses in the town of Tamaqua.

A PPENDIX

C

LITTLE SCHYULKILL DAM CHECK LIST HYDROLOGIC AND HYDRAULIC ENGINEERING DATA

DRAINAGE AREA CHARACTERISTICS: 90 % wooded, mountainous, sparsly populated
ELEVATION TOP NORMAL POOL (STORAGE CAPACITY): none- a "dry" dam
ELEVATION TOP FLOOD CONTROL POOL (STORAGE CAPACITY): 1116.6 (5940 Ac-Ft top of dam)
ELEVATION MAXIMUM DESIGN POOL: 1113.3 (4940 Ac-Ft)
ELEVATION TOP DAM: 1116.6
EMERGENCY SPILLWAY:
a. Elevation 1103.0
b. Typerock channel
c. Width 200 feet
d. Length 300 feet along centerline
e. Location Spillover right abutment
f. Number and Type of Gatesnone
PRINCIPAL SPILLWAY:
a. Type _concrete riser, 48" concrete conduit and impact basin
b. Location 150 feet from left abutment
c. Entrance inverts 1028.0 and 1048.0
d. Exit inverts 1024.9
e. Emergency draindown facilities through ungated orfice at 1028.0
HYDROMETEOROLOGICAL GAGES:
a. Type none
b. Location
c. Records
MAXIMUM NON-DAMAGING DISCHARGE: not determined

The same of the sa

DAM SAFETY ANALYSIS HYDROLOGIC/HYDRAULIC DATA

Date: 6/85/78 By: <u>MFB</u> Sheet: <u>2</u> of <u>5</u>

DAM Little Schuylkill Dam Nat. ID No. PAOOGS5 DER No. 54-174

	ITEM/UNITS	Permit/Design Files (A)	Calc. from Files/Other (B)	Calc. from Observations (C)
1.	Min. Crest Elev., ft.		1116.6 #	
2.	Freeboard, ft.			
3.	Spillway ⁽¹⁾ Crest Elev, ft.	1048 Ft.	1048 Pt	
3a.	Secondary ⁽²⁾ Crest Elev, ft.	1103H	11034	
4.	Max. Pool Elev., ft.	1111.3 #		
5.	Max. Outflow ⁽³⁾ , cfs	37,500cfs		
6.	Drainage Area, mi²	15.58 mile	15.50 mile 2	14.69 mile 2
7.	Max. Inflow $^{(4)}$, cfs			
8.	Reservoir Surf. Area, ft ²			
9.	Flood Storage ⁽⁵⁾	3698 Ac-F+	369BAc-Ff	
10.	Inflow Volume, ft ³			

Reference all figures by number or calculation on attached sheets:

Example: 3A - Drawing No. xxx by J. Doe, Engr., in State File No. yyyy.

NOTES:

- (1) Principal spillway
- (2) Emergency spillway
- (3) At maximum pool, with freeboard, ungated spillways only.
- (4) For columns B, C, use PMF.
- (5) Between lowest ungated spillway and maximum pool.

Date: 6/45/78 By: MFB Sheet: 3 of 5

HYDROLOGIC/HYDRAULIC CALCULATIONS (cont.)

Item (from sheet 2)

Source

3A, 3a A, 4A, 5A. 6A, 9A

Application Report dated June 2, 1966

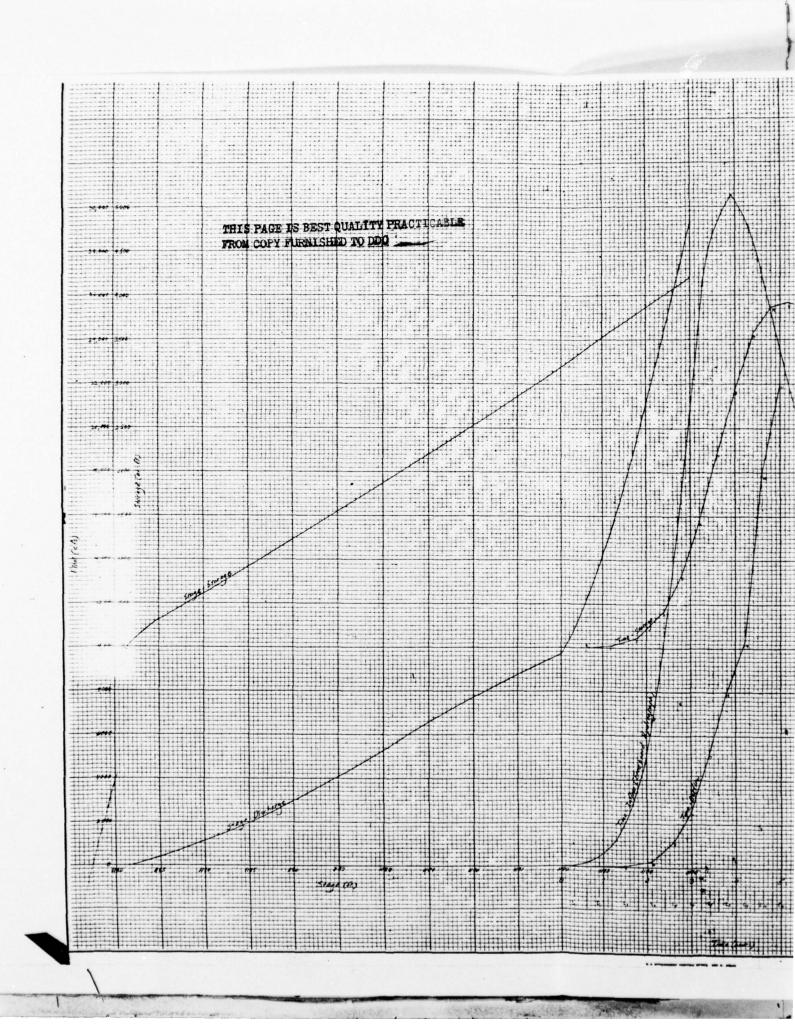
6C

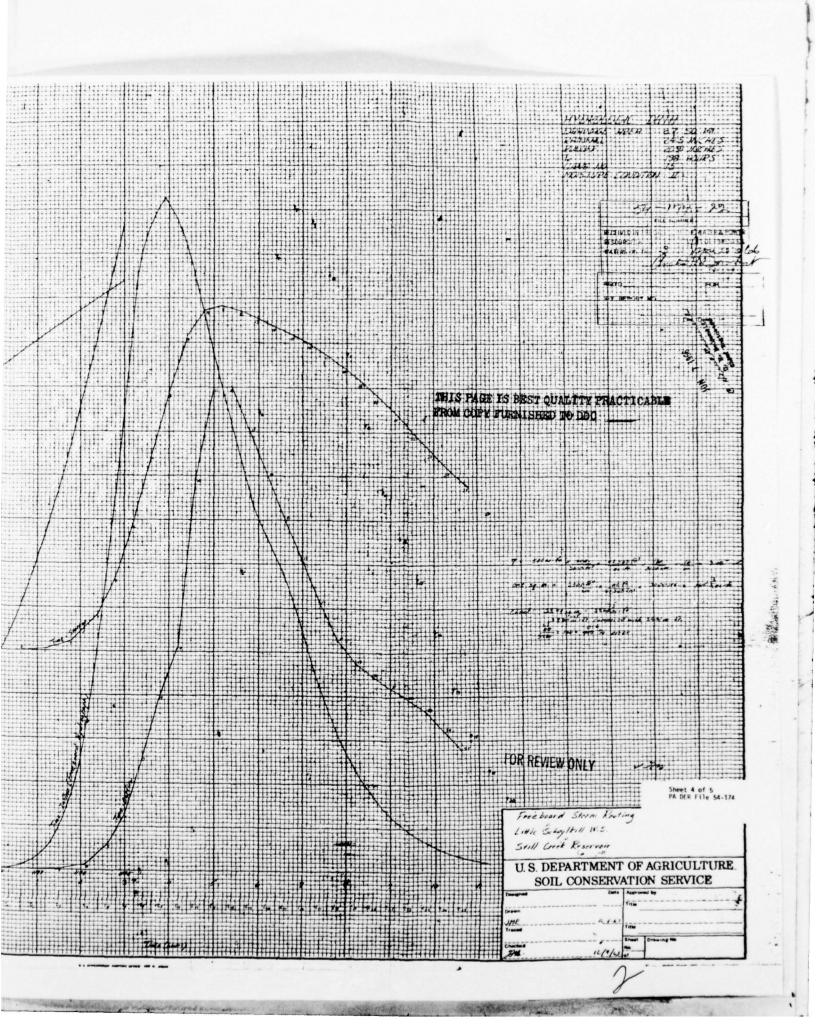
USG3 Haps 6.9 mile 2 Still Greek Reservoir 7.79 mile Intervening Area Delano (1969)

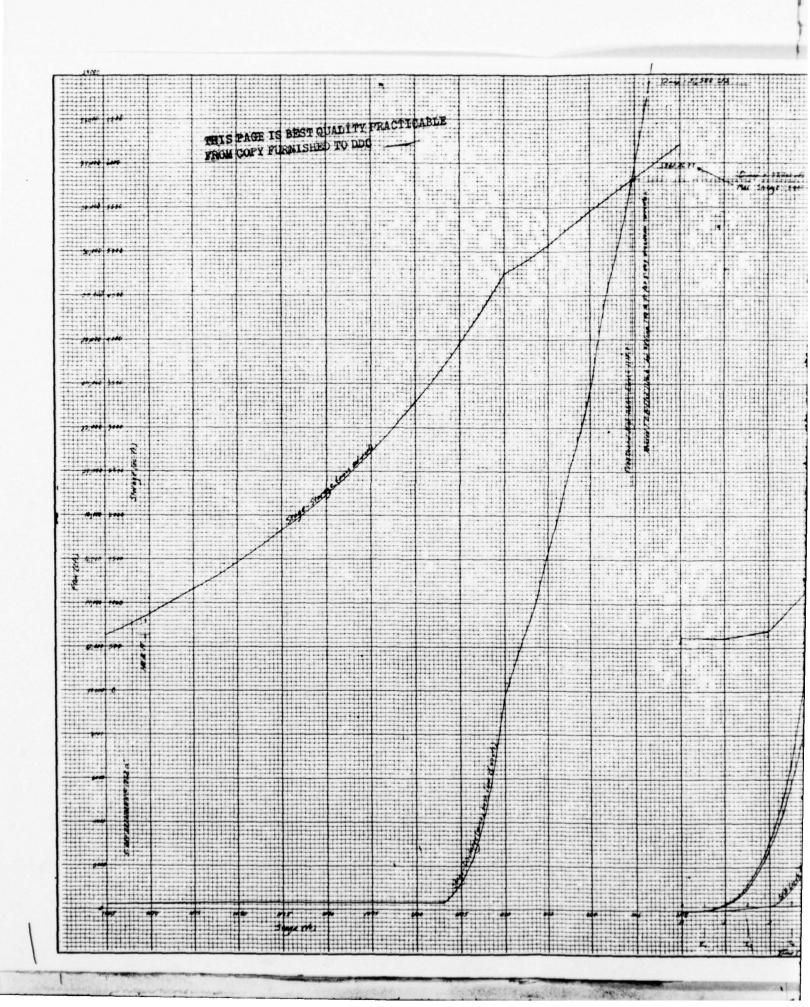
Conyngham (1969) Tamaqua (1976) Hazelton (1969)

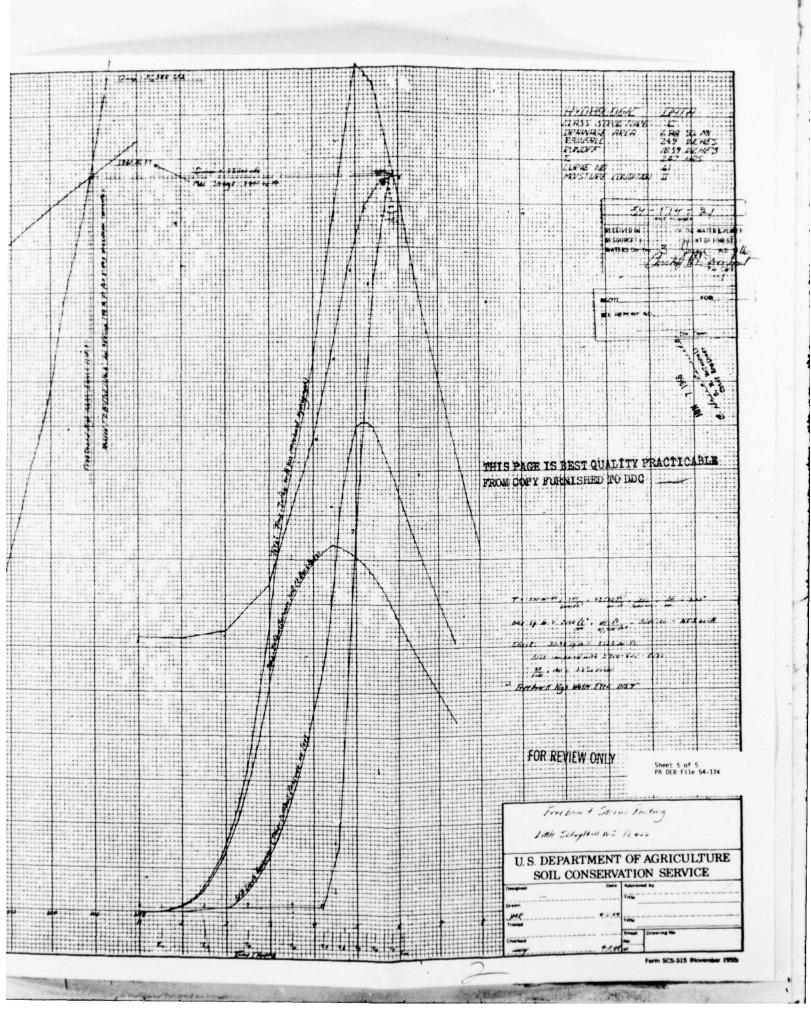
18, 38, 328, 68,98

Construction Drawings dated June 1966









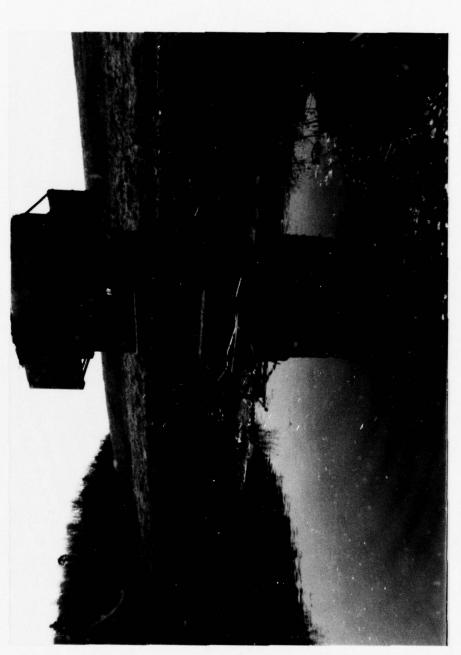
APPENDIX

D

The second second

VIEW FROM RIGHT ABUTMENT. UPSTREAM SECTION IS ON LEFT SIDE OF PHOTO AND EMERGENCY SPILLWAY CHANNEL IS IN FOREGROUND.

PHOTO NO. 1



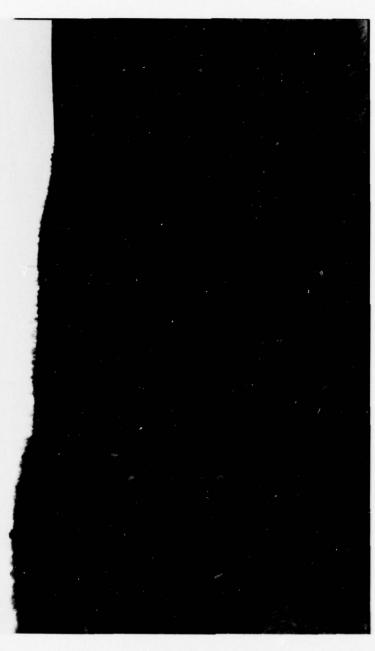
PRINCIPAL SPILLWAY ENTRANCE WITH TWO INTAKE LEVELS. NOTE TRASH ACCUMULATION AT ENTRANCE OF LOWER INTAKE.



PRINCIPAL SPILLWAY OUTFALL STRUCTURE AND STILLING BASIN. THE PIPE DISCHARGES WATER AGAINST A BAFFLE WALL (SHOWN) AND THE WATER PASSES UNDER AND THROUGH NOTCHES ON EACH SIDE OF THE WALL.

VIEW OF EMERGENCY SPILLWAY AND RIGHT WALL OF SPILL-WAY CHANNEL. THE ROCK FACE CONSISTS OF SOUTH DIPPING SANDSTONE AND SHALE OF THE MAUCH CHUNK FORMATION.

PHOTO NO. 4



VIEW LOOKING DOWN THE EMERGENCY SPILLWAY CHANNEL WHICH ENTERS INTO THE STREAM BELOW. THE SOIL MANTLE WHICH SUPPORTS THE GROWTH OF GRASS IS VERY THIN.



VIEW LOOKING DOWNSTREAM. NOTE RAILROAD BRIDGE DOWNSTREAM.



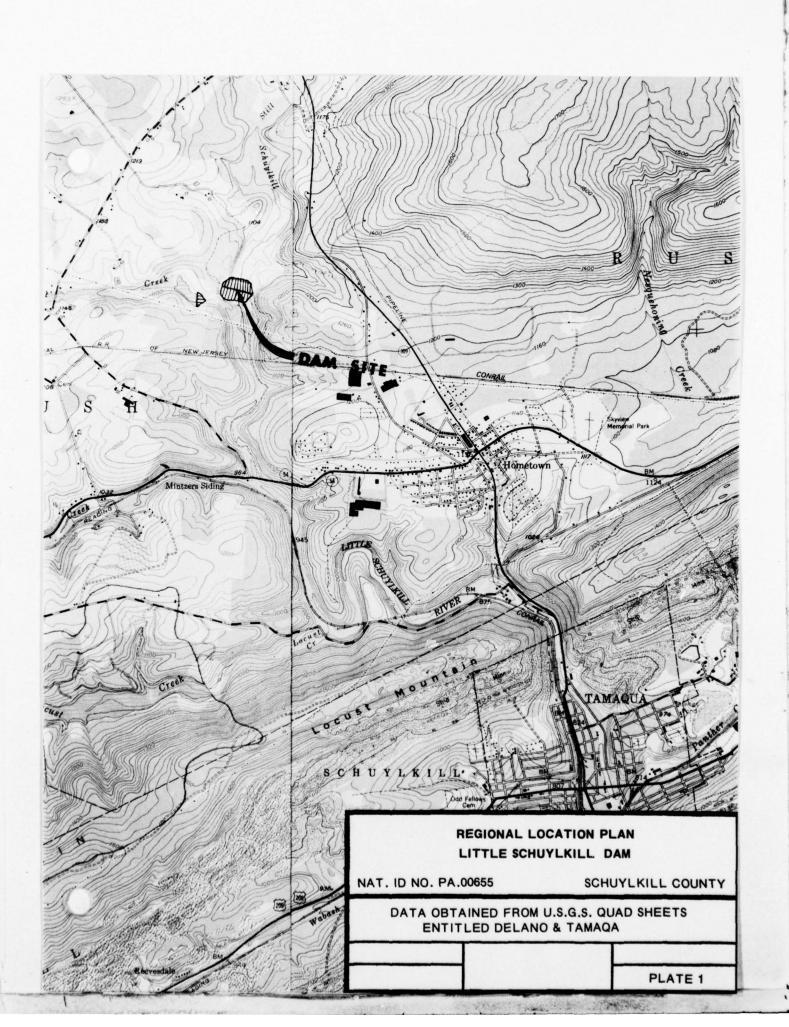
VIEW LOOKING ACROSS EMERGENCY SPILLWAY TORWARD THE DAM. UPSTREAM SECTION OF DAM IS ON LEFT. NOTE TRIPLE LINE GROUT CURTAIN PIPES INDICATED BY GEOLOGIC HAMMER, FLASHLIGHT AND INSPECTOR.

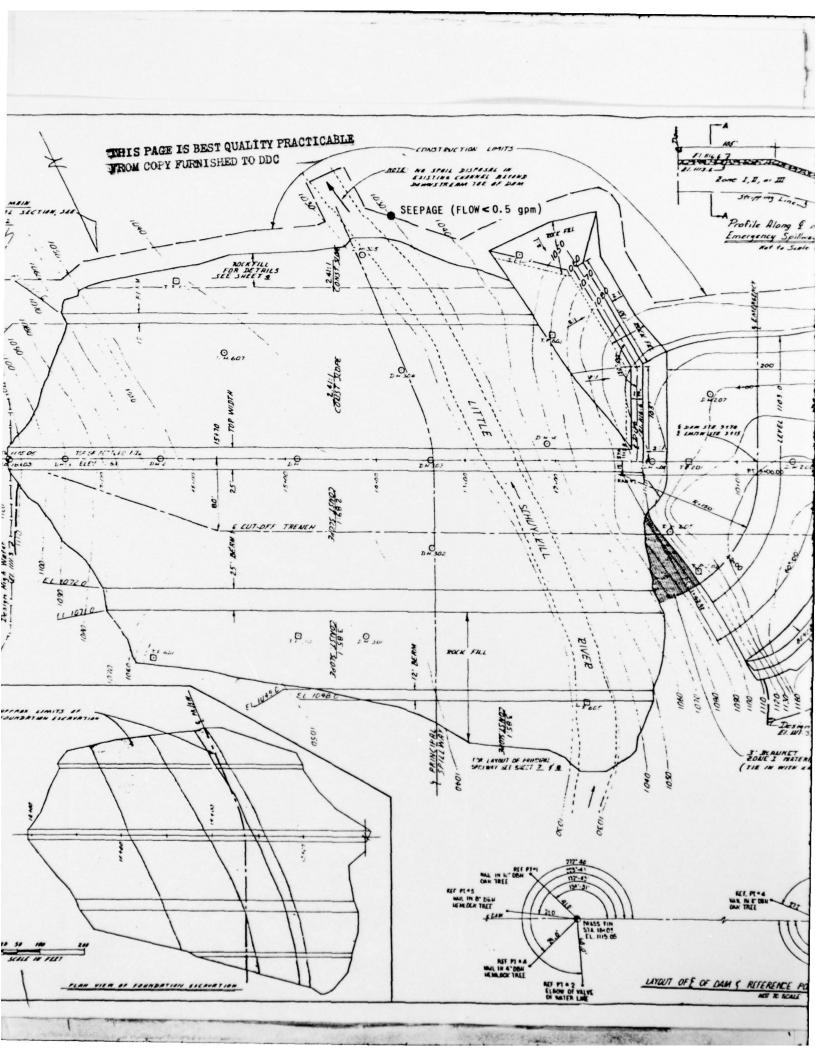


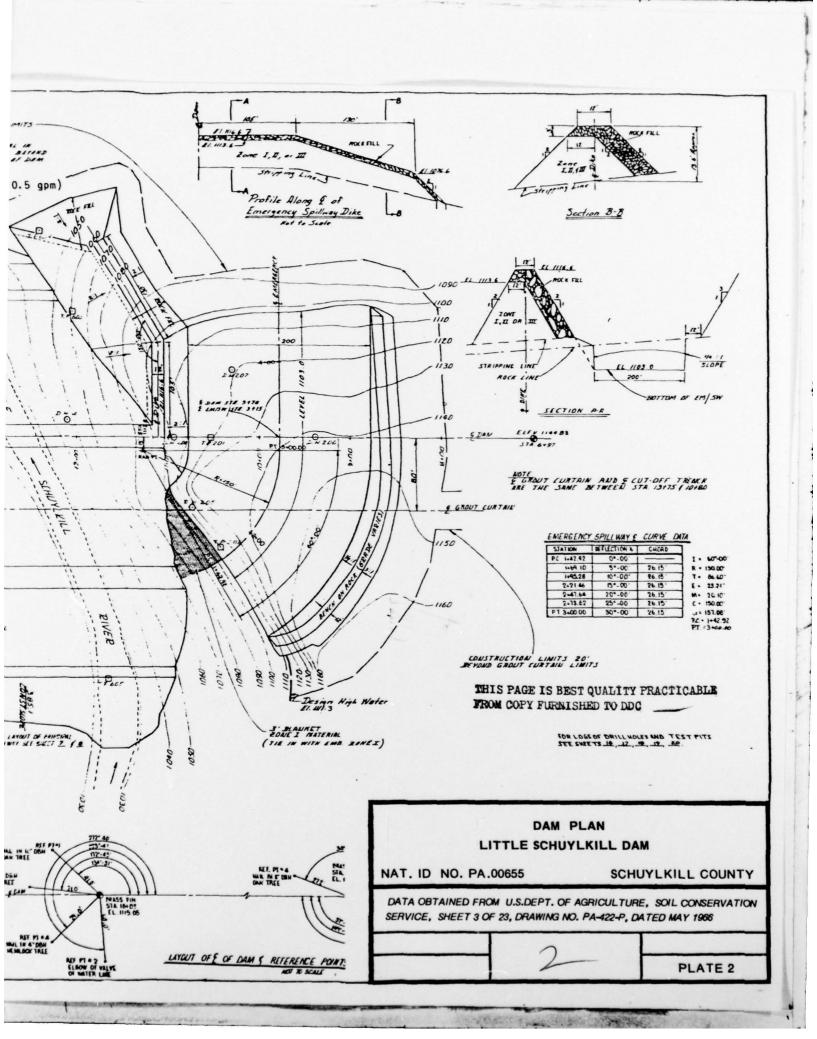
VIEW OF ONLY SEEPAGE NOTED ON THE DOWNSTREAM SLOPE. EMERGENCE CAN BE SEEN IN CENTER OF PHOTO WHERE MOSS GROWTH DEVELOPED.

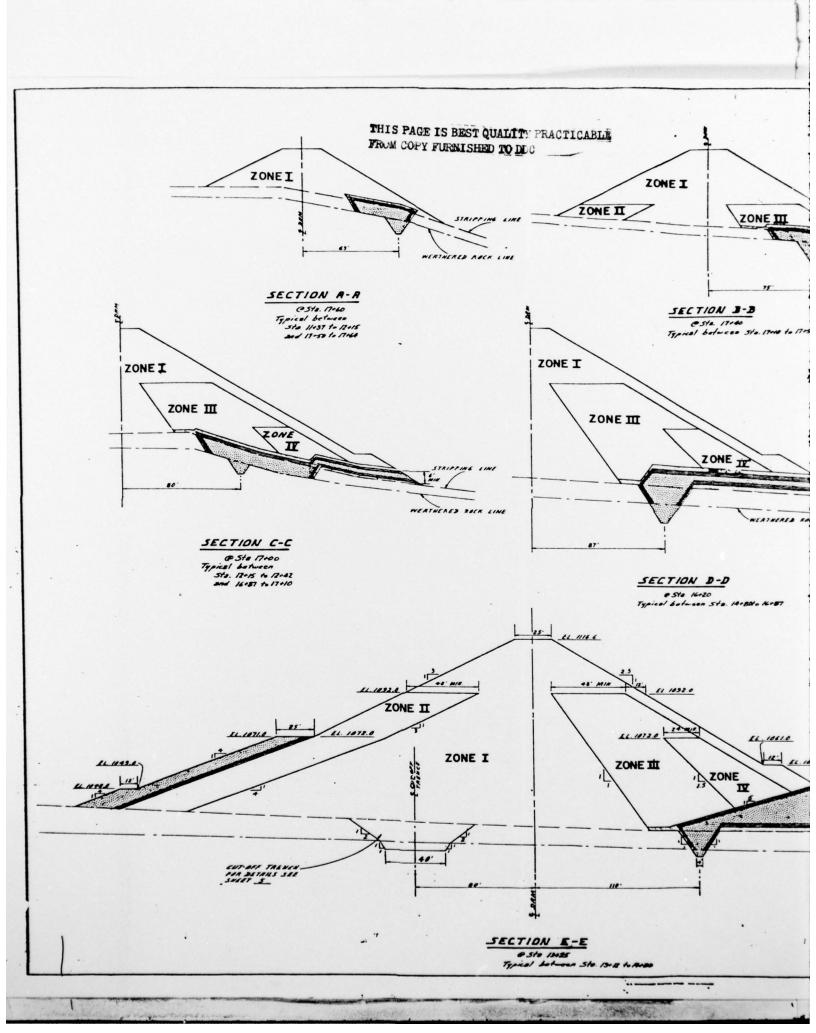
APPENDIX

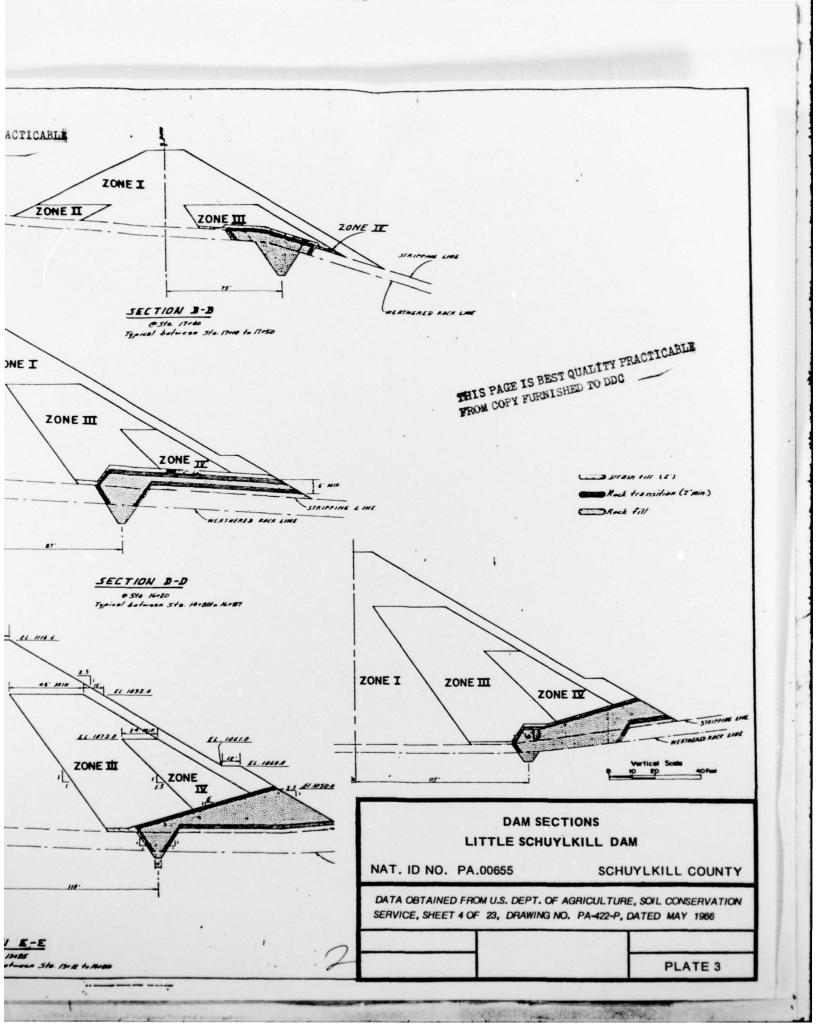
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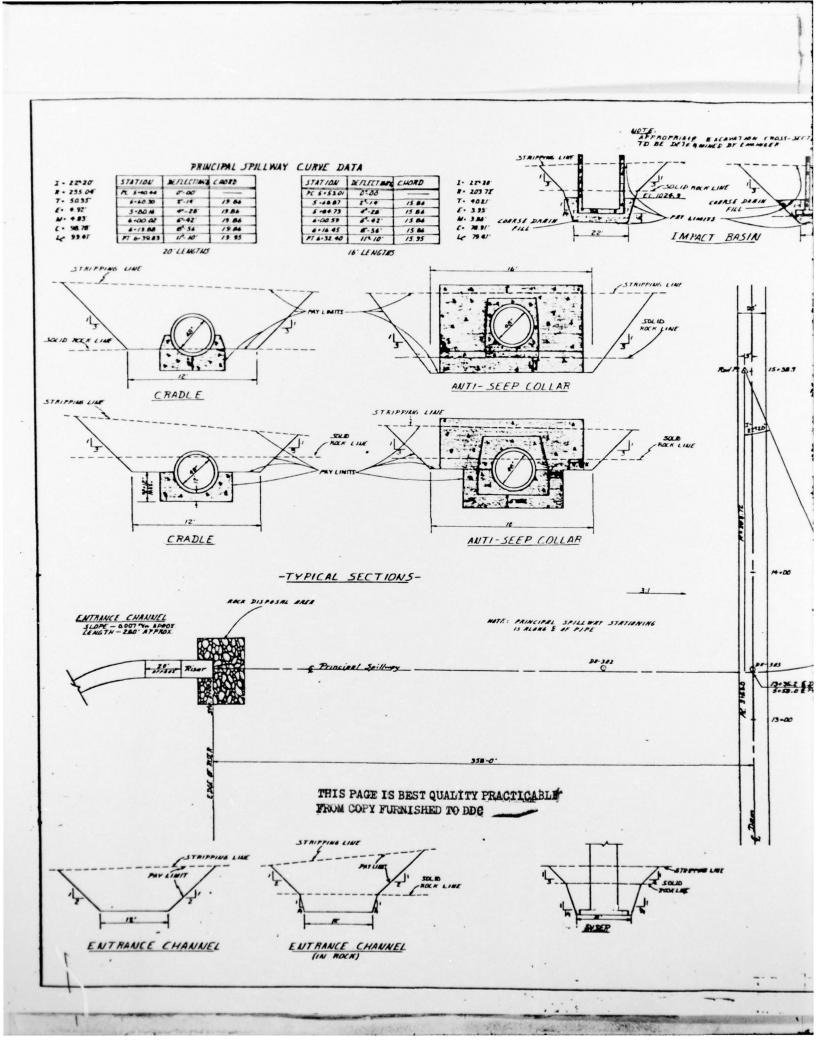


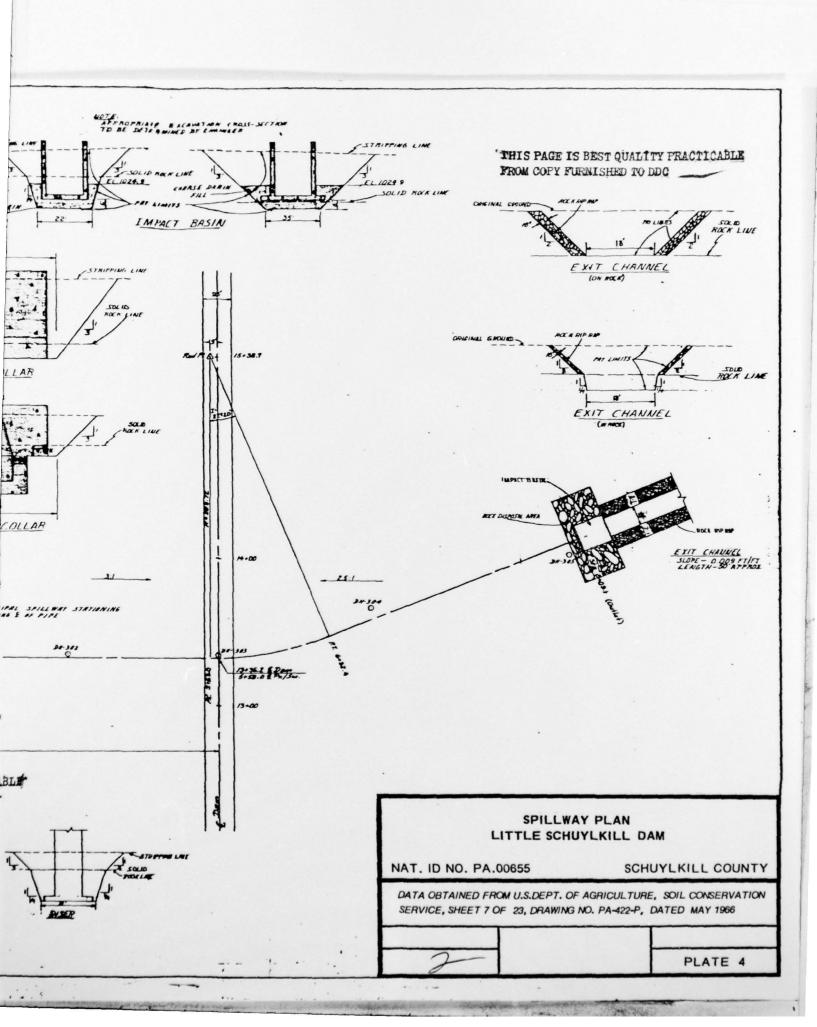


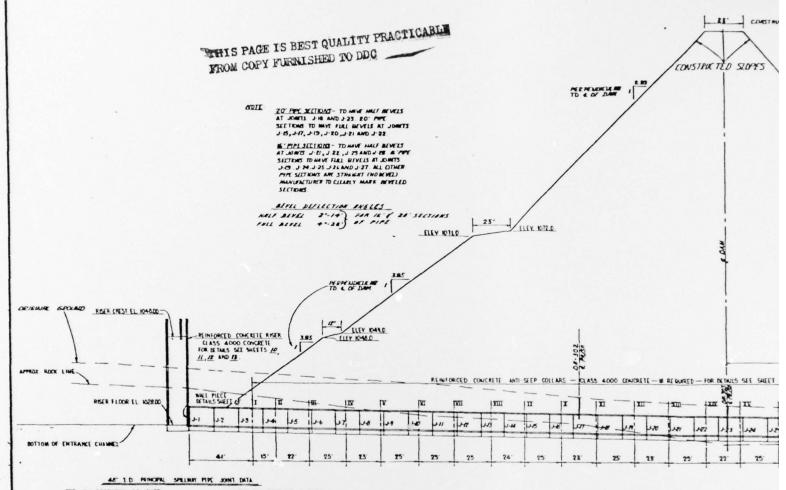












FOR 16" SECTIONS OF PIPE

FOR 20 SECTIONS OF PIPE

TREMETH CLASS	THIOL	RISER WALL	FLEVATION
1	J-1	0.3	1016.00
	J-2	16.4	1088.00
1 1	1-3	32.5	1028.00
1	1-4	46.5	101 B.00
1 1	15	64.6	1026.00
! 1	1-6	80.6	109 8.00
1 1	J-7	96.7	1018.00
1	J-6	112.8	1078 00
1 1	1-4	128.6	1088.00
1 1	J-10	144.4"	1018.00
1 1	J-11	160.4	1028.00
11	J-12	177.0	1016.DC
1	J-13	193.1"	1028.00
1 1	1-14	109.1	IOR B.OC
7 1	J-15	225.2	1028.00
H	J-16	241.2	1028.00
1 1	J-17	£57.8"	1028.00
1	3-18	273.4	1028.00
1	1-19	2M.2'	1028.01
1 1	1-20	302.9	1026.7
	J-21	321.1	1025.5
	J-22	337.1	1024.4
W	J-23	253.0	1074 9
1	J-24	368.4	1024 9
	J-25	384.7	1024.9
	J-26	400 6	10744
1	J-77	416.5	1074.9
1	J-26	4324	1024.9
H	J-79	448.5	1024 4
-	J-30	464.5	1074 9
	1-31	480.6"	1024.9
-	J-37	476.6	1004.9
1	1-33	5127	1024.9
	1-34	578.6	1074.9
:	J-35	3448	1074.4
1	J-36	240.4.	1024.9
	J-97	574.9"	1004.9
1	J-06	5410	1024 4
+	CHILET	POT 1.	1004.9

THIOL	DETANCE FROM		STRE NGT
JOHN	RISER WALL	ELEVATION	CLASS
J-1	0.2	10766	
1-2	204	102 8.00	1
7-2	40.4	102800	1 1
1-4	60.5	10 28 00	1 1
1.5	80.5	1028.DO	1
1-6	1005	1028.00	İ
1-7	120.6	102.B.00	1 1
J-8	140.6	00.830	1
1-4	160.F	1028.00	1
J-10	180 T	1028.00	1
J-11	200.7	1028.00	11
J-12	2205	1028.00	1 1
J- 13	1400	1028.00	П
J-14	2.603	1028.00	1
J-15	7807	105600	1 +
J-16	300.7	1026.45	11
J-17	3265	1024.90	1 1
J-18	374	102450	1 1
1-19	3603	107490	Ш
J-20	3802	102490	1 1
J-21	4000	102450	1
J-22	4/99	10Z+90	11
J-23	439.8	WZ+30	11
J-24	4599	102990	11
J-25	479.9	102490	1 7
J-26	6000	1024:90	11
J-27	5200	102430	1 1
J-28	6400	102490	1
1-27	5601	1024.90	1 ;
J-30	5BQI	102490	11
J-31	6001	102490	1
OUTLET	Wal	102430	1 1

PROFILE OF PRINCIPAL SPILLWAY

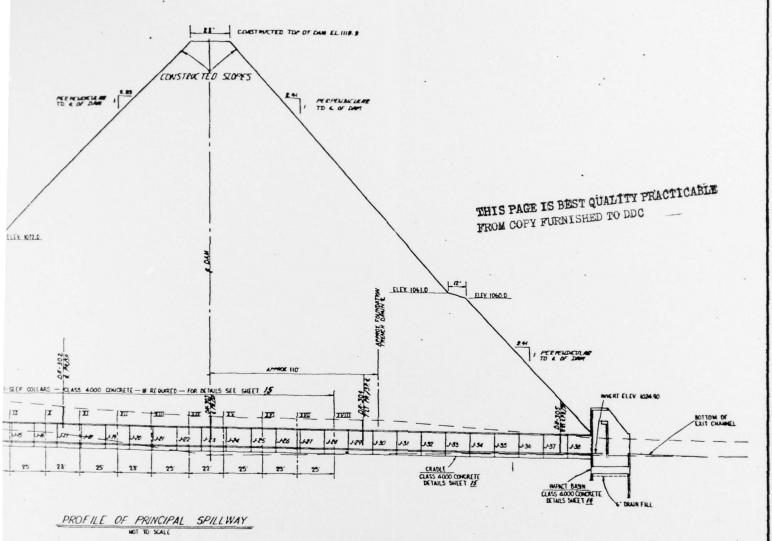
PRINCIPAL SPILL WAY ANTI-SETP COLLAR DATA

FOR 16" SECTIONS OF PIPE

FOR 20' SECTIONS OF PIPE

COLLAR	RISER WALL	ELEWATION
1	41.0	1028.00
п	56.0°	1028.00
II	76.0	1028.00
M	103 0	1028.00
I	126.0	108 8 00
Y	151.0	102E .00
YII	114.0	106 9 901
XII	199.0	102 8.00
п	223.0	1028 00
I	246.0	1028.00
I	271.0	1028.00
III	296.0	1027 47
III	319.0"	1025.67
IN	344.0"	1084.90
IV	364.0	1014.90
IVI	341.0	1074 90
THE	4 M.D'	1074.4
IVE	439.0	1024.90

COLLAR	DISTANCE FROM	ELEVATION
1	43.0	1028.00
II	68.0	1028.00
m	95.0	1028.00
N	116.0	1028.00
¥	145.0	1028.00
ZI	168.0	1018.00
MI	1930	1028.00
VIII	R18.0	1028.00
IX	243.0	1078.00
I	569.0	1028.00
I	293.0	1027.05
III	318.0	1075.09
XIII	348.0	1024 90
XIX	368.0	1024.40
XX	393.0	1024.40
XV	417.0	1074 . 00
TAI	442.0	1024 40



MOTE: PROFILE OF PRINCIPAL SPILLWAY SHOWN IS BUSED ON DATA FOR 16" SECTIONS OF CONDUIT.

SPILL WAY ANTI- SEEP COLLAR DATA

PIPE FOR 20 INVERT COLLAR INST

00.850

28.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78.00 78

FOR	20	SECTIONS	OF	PIPE	

COLLAR	DISTANCE FROM	INVERT ELEVATION
1	43.0	1028.00
II	68.0	1028.00
E	95.0	1028.00
N	116.0	1028.00
¥	145.0	102 8.DO
V	168.0	1028.00
W	193.0	1028.00
YIII	218.C	1028.00
II	243.0	1028.00
I	268.0	1028.00
II	293.0	1027.05
III	318.0	1075.09
III	348.0	1024.90
XIX	368.0	1024.40
IY	393.0	1024 NO
IV	417.0	1074 . 40
TAI	442.0	1024 90

SPILLWAY SECTION
LITTLE SCHUYLKILL DAM

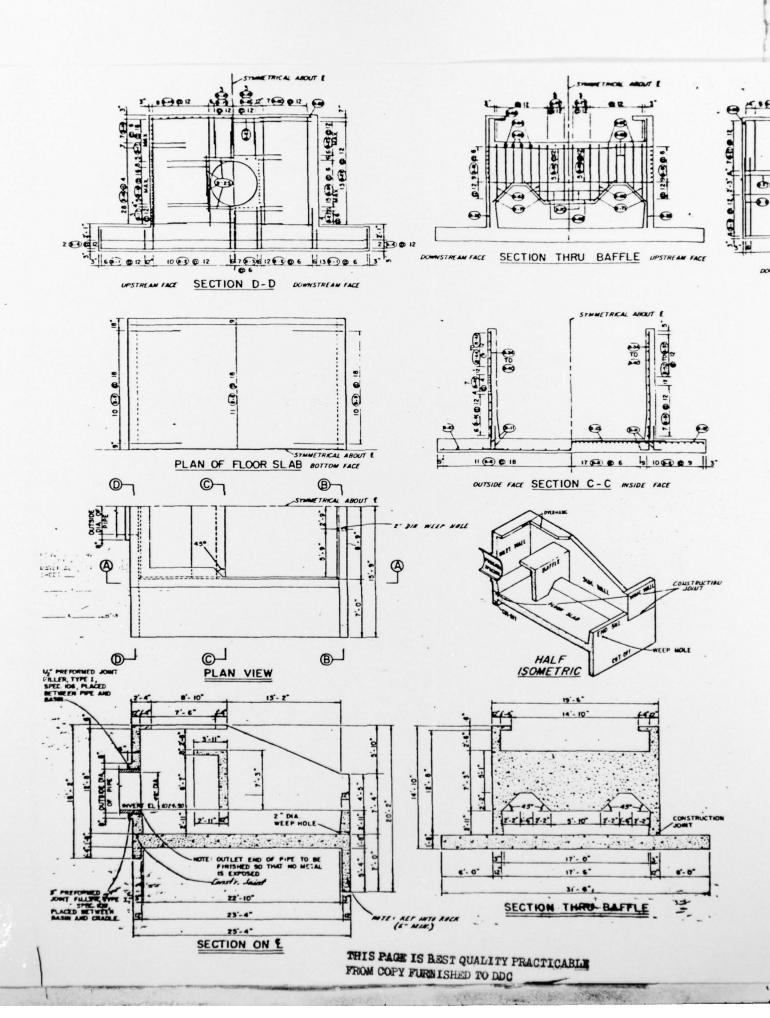
NAT. ID NO. PA 00655

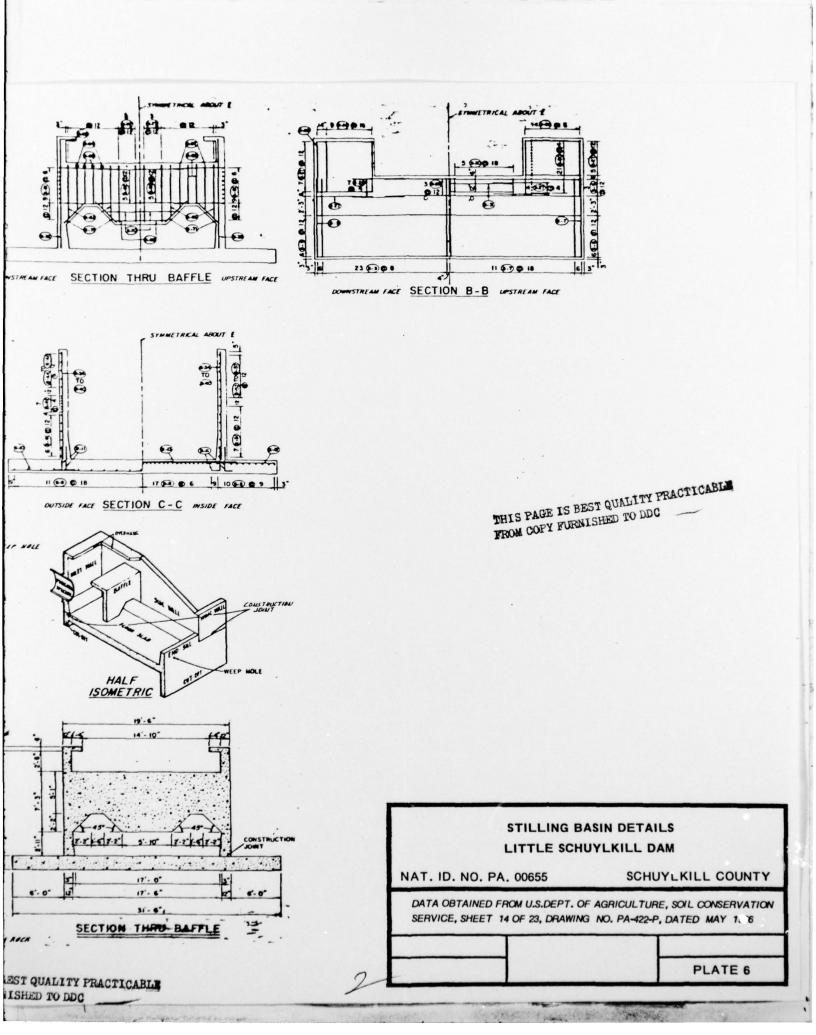
SCHUYLKILL COUNTY

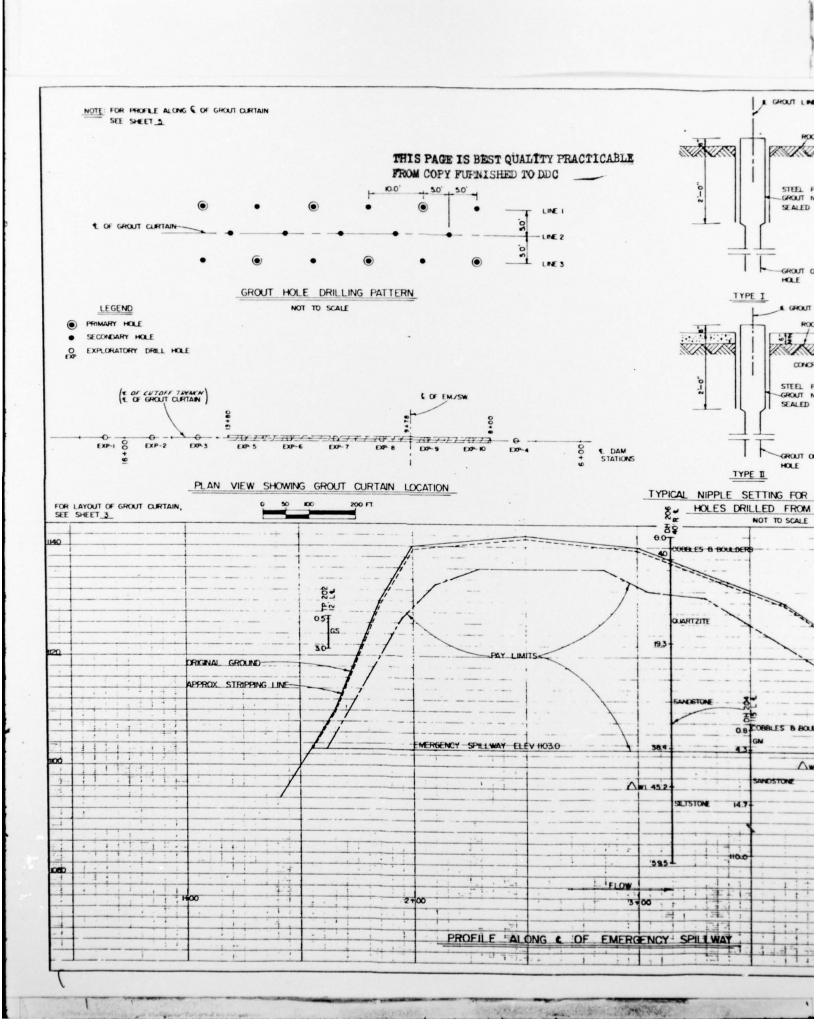
DATA OBTAINED FROM U.S.DEPT. OF AGRICULTURE, SOIL CONSERVATION SERVICE, SHEET 8 OF 23, DRAWING NO. PA.422-P, DATED MAY 1966

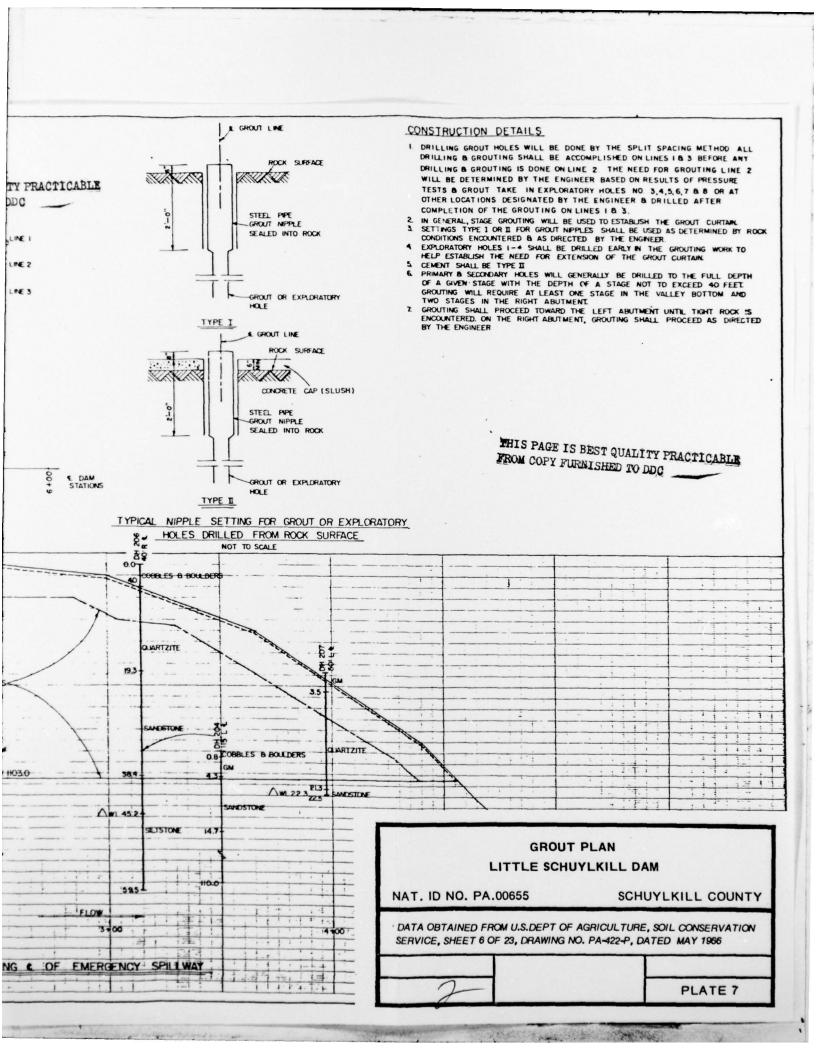
PLATE 5

2-









APPENDIX

F

SITE GEOLOGY LITTLE SCHUYLKILL DAM

Little Schuylkill Dam is located in the Appalachian Mountain Section of the Valley and Ridge Physiographic Province. As shown in Plate F-1, the dam is located in the sandstone and shale of the Pocono and Mauch Chuck formations of Mississippian age. The entire dam structure is founded in the Pocono Formation except for the right abutment which is underlain by the Mauch Chunk Formation (see Photo No. 4). In the right abutment area, bedrock strikes west-northwest and dips approximately 20 degrees to the south (downstream direction). Jointing strikes northwest and dips 70 degrees to the southwest (downstream direction (and 65 degrees to the northeast. Another major joint set strikes east-northeast with near-vertical dips to the north.

The dam lies between two regional east-northeast trending folds in an area of localized thrust faulting. Several faults occur in the immediate dam foundation area as shown on Plate F-1. One is a low angle thrust fault with an elliptical fault trace due to erosion which formed the present Little Schuylkill River valley. The other fault which terminates near the right abutment strikes east-northeast with a sense of movement of down-to-the-south.

The combination of southerly dipping bedding and joint planes and faulted terrain would be conducive to downstream water seeps. Problems of water seepage are not considered to be significant since this dam is a flood control structure and is not expected to be at maximum capacity for extended periods.

